

Mole concept

$$1) \quad n_A = \frac{W_A}{M_A} = \frac{\# \text{ particles}}{6.02 \times 10^{23}} = \frac{\text{Vol (A)}}{22.4 \text{ l/mol}}$$

$$2) \text{ Avg. molecular wt.} = \boxed{\frac{W_{\text{Total}}}{n_{\text{Total}}}}$$

$$3) \text{ Vapor Density} = \left(\frac{M_A}{2}\right)$$

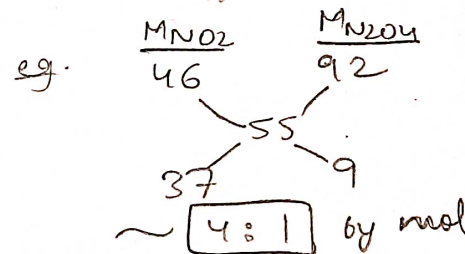
$$4) \quad \% \text{ mass} = \frac{W_{\text{element}}}{W_{\text{Total}}} \times 100\%$$

$$5) \quad \% \text{ mol} = \frac{n_{\text{element}}}{n_{\text{Total}}} \times 100\%$$

$$6) \quad (M.F.) = (E.F.)n$$

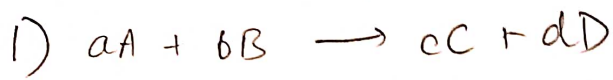
$$7) \quad n = \left(\frac{M.F. \text{ mass}}{E.F. \text{ mass}}\right)$$

★
In questions, prefer to use mixture & Alligation Trick



★ In questions about finding EF, if %s of given elements don't add up to 100% \Rightarrow Rest of the element is Oxygen(O)

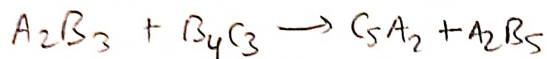
Stoichiometry



Balanced Chem. Rxn,

$$\frac{n_A}{a} = \frac{n_B}{b} = \frac{n_C}{c} = \frac{n_D}{d}$$

2) POAC



$$3n_{A_2B_3} + 4n_{B_4C_3} = 5n_{A_2B_5}$$

$$3) \% \text{ yield} = \frac{W_{\text{actual}}}{W_{\text{expected}}} \times 100\%$$

$$4) \% \text{ purity} = \frac{W_{\text{pure}}}{W_{\text{impure sample}}} \times 100\%$$

5) Limiting Reagent

Compare $\left(\frac{n_A}{a}\right)$.

Reactant with lower $\left(\frac{n_A}{a}\right)$ is the LR.

$$5) m = \frac{n_B}{W_A} \text{ (in kg)}$$

$$6) \text{ppm} = \frac{W_B}{W_S} \times 10^6 \\ \sim \frac{W_B \times 10^6}{W_A}$$

$$7) N = \frac{\text{eq}(B)}{V_S} \text{ (in L)}$$

Relations b/w Conc. Terms

$$- N = M \times n_f$$

$$- \text{eq.} = \text{mol} \times n_f$$

$$- \% \text{ w/v} = \% \text{ w/w} \times d_s$$

$$- M = \frac{\% \text{ w/v} \times 10}{M_B}$$

$$- M = \frac{(\% \text{ w/w}) (d_s) \times 10}{M_B}$$

$$- m = \frac{1000 M}{1000 d_s - M M_B}$$

$$- m = \frac{1000 \chi_B}{M_A \chi_A}$$

$$- M = \frac{1000 d_s \chi_B}{M_A \chi_A + M_B \chi_B}$$

Concentration Terms

A \rightarrow solvent
B \rightarrow solute
S \rightarrow soln

$$1) \% \text{ v/v} = \frac{V_B}{V_S} \times 100\%$$

$$2) \% \text{ w/v} = \frac{W_B}{V_S} \times 100\% \text{ (100 ml)}$$

$$3) M = \frac{n_B}{V_S} \text{ (in L)}$$

$$4) \chi_B = \left(\frac{n_B}{n_A + n_B}\right)$$

$$\star \sum \chi_i = 1$$

Dilution & Mixing

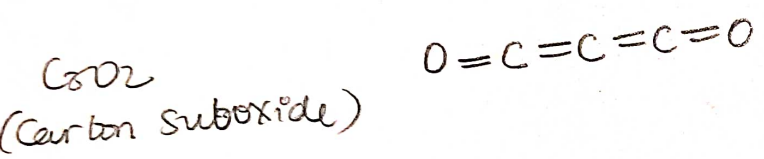
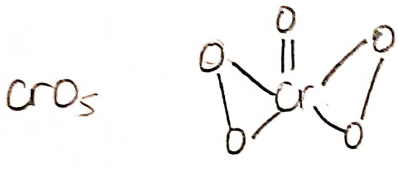
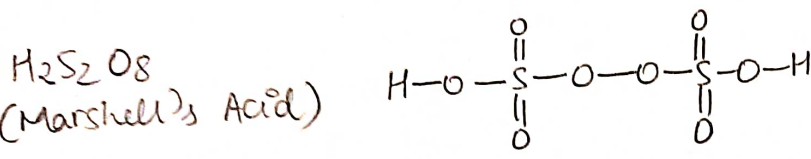
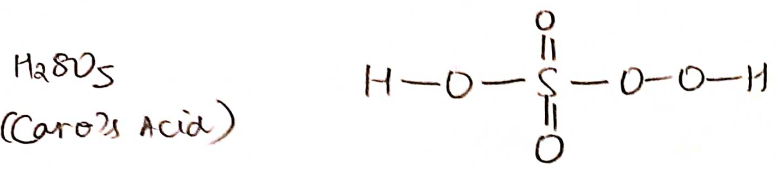
$$1) M_1 V_1 = M_2 V_2$$

$$2) M_1 V_1 + M_2 V_2 = M_f V_f$$

$$\star V_f = V_1 + V_2 \text{ if } \rho_A = \rho_B$$

$$\text{On general } \rho_1 V_1 + \rho_2 V_2 = \rho_f V_f$$

Redox Reactions



Balancing Redox Rxns

① Ion- e^- : O by H_2O
H by H^+
 e^- for conserving charge

② Oxid. no. : Cross Multiply #e⁻ exchanged in Oxid & Red sides

③ Algebraic Eqn. Method :
- Add coeffs a, b, c, ... to skeletal rxn chems.
- Use POAC & conserve charge (on all elems)
- Assume any one of the coeffs to be 1.

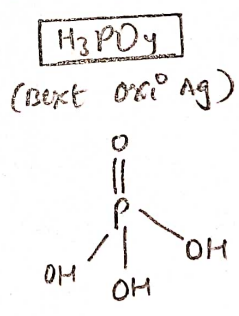
Equivalent Concept

n-factor - Charge transferred per mol of specie

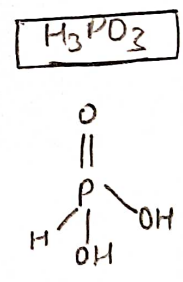
- ① Ions : Charge on Ion
- ② Salts : Total +ve charge on Cation
- Mohr's Salt - $FeSO_4 \cdot (NH_4)_2SO_4 \cdot 6H_2O$
- Potash Alum - $K_2SO_4 \cdot Al_2(SO_4)_3 \cdot 24H_2O$

- ③ Acid - Basicity (in rxn)
- ④ Bases - Acidity (in rxn)

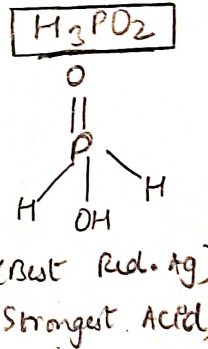
Exceptions



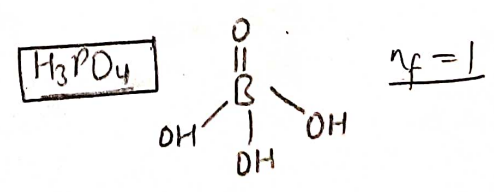
$n_f = 3$



$n_f = 2$

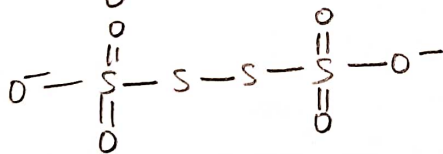
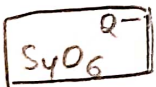
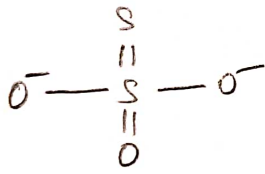
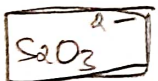
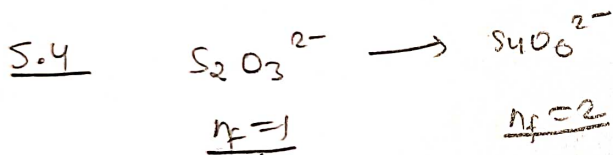
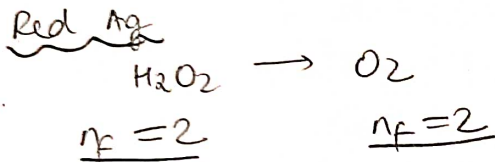
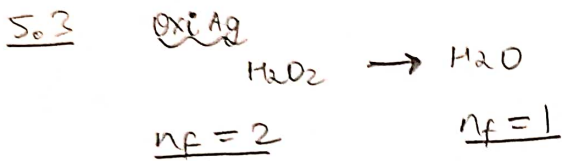
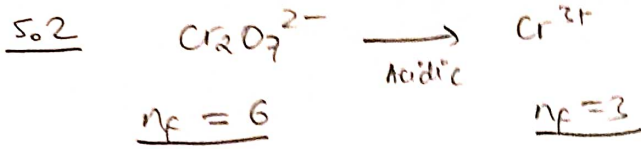
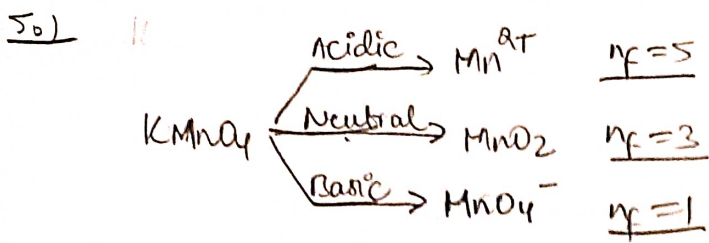


(Best Red. Ag)
(Strongest. Acid)
 $n_f = 1$

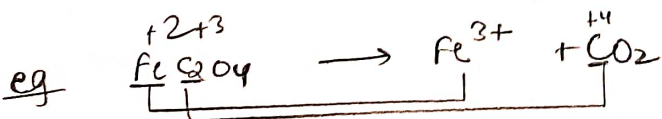


$n_f = 1$

⑤ Oxid & Red Ag. - (Intermolecular)



Special Case : More than one atom undergoing oxidation/reduction



$$n_f(\text{FeC}_2\text{O}_4) = n_f(\text{Fe}) + 2n_f(\text{C}) = (1 \times 1) + (2 \times 1) = 3$$

n₁ → # e⁻ transferred in oxi
n₂ → # e⁻ transferred in Red

⑥ Oxi & Red Ag. - (Intramolecular)

Case I - n₁ = n₂

$$n_f = n_1$$

Case II - n₁ ≠ n₂

$$n_f = |n_1 - n_2|$$

NOTE: All elems. which are undergoing Red/Ox must be balanced to calculate n₁ & n₂

⑦ Oxi & Red Ag - (Disproportionation)

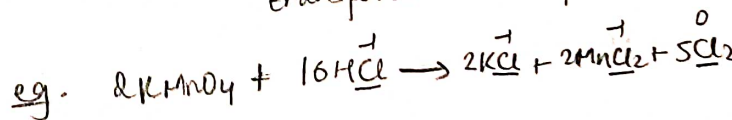
$$n_f = \frac{n_1 \times n_2}{n_1 + n_2}$$

⑧ General Method

- Balance rxn using ion-e⁻ method

$$n_f(A) = \frac{\#e^- \text{ involved}}{\text{coeff.}(A)}$$

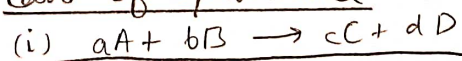
*** Special Case : When an element is not wholly transferred in 1 product.



$$16\text{HCl} \rightarrow 10e^-$$

$$\rightarrow n_f(\text{HCl}) = \frac{10}{16} = \left(\frac{5}{8}\right)$$

⑨ Law of Equivalence



$$\text{eq}(A) = \text{eq}(B) = \text{eq}(C) = \text{eq}(D)$$

(ii) in a compound M_mN_n

$$\text{eq}(M_mN_n) = \text{eq}(M) = \text{eq}(N)$$

$$\begin{aligned}
 (\% \text{ Alum strength}) &= \frac{\text{Wt. (H}_2\text{SO}_4)_{\text{initial}}}{\text{Wt. (H}_2\text{SO}_4)_{\text{initial}} + \text{Wt. (H}_2\text{SO}_4)_{\text{produced by free SO}_2}} \\
 &= (100 - 40) + 49 = \boxed{109\%}
 \end{aligned}$$

In General,

$$\frac{\text{Wt (SO}_2)}{80} = \frac{(\% \text{ Ol. Str.} - 100)}{18}$$

Wt. of SO₂ in 100g of alum

NOTE: $\frac{(\% \text{ Alum str.} - 100)}{\uparrow}$ Wt. of H₂O added to convert SO₂ → H₂SO₄ per 100g alum.

→ Ion-Exchange-Resin Process (Demineralised Water) (6)

NOTE: Hardness of any substance is calculated w.r.t CaCO₃.

$$\text{eq. (m)} = \text{eq. (CaCO}_3)$$

$$(\text{Degree of Hardness}) = \frac{\text{Wt. (CaCO}_3) \times 10^6 \text{ ppm}}{\text{Wt. (soln)}}$$

Available Chlorine

$$(\% \text{ available Cl}) = \frac{\text{Wt. (Cl released)}}{\text{Wt. sample}} \times 100\%$$

Hardness of water

- Temporary - Bicarbonates of Ca²⁺ & Mg²⁺
- Permanent - Cl⁻ & SO₄²⁻ of Ca²⁺ & Mg²⁺

Ways to Remove

- Temporary
- Heating
 - Clark's Process (adding Ca(OH)₂)
 - Addⁿ of Na₂CO₃

- Permanent
- Permutit Process
(Na₂Z = Na₂Al₂Si₂O₇ · nH₂O)
zeolite Sodium Aluminosilicate
 - Calgon's Process
(Na₂[Na₄P₂O₇])
(Sodium Hexa-meta phosphate)
 - Na₂CO₃ & Na₃PO₄

ATOMIC STRUCTURE

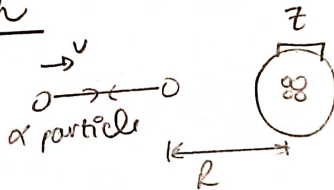
Rutherford & Before

Cathode Rays — C → A
 e/m ratio const. called e^- .

Anode Rays (Canal) — A → C
 e/m ratio varies

	e	p	n
Mass	9.1×10^{-31}	1.67×10^{-27}	1.67×10^{-27}
Charge	-1.6×10^{-19}	$+1.6 \times 10^{-19}$	0

Closest Approach



At closest dist,

$$KE_{\text{initial}} = P.E \Rightarrow \frac{1}{2}mv^2 = \frac{k(2e)(Ze)}{R}$$

Bohr's Model

$$mvr = n\hbar$$

$$E = \frac{12400}{\lambda} \text{ (in eV)} \quad (E = h\nu) \text{ in general}$$

for one photon

$$1 \text{ eV} = 1.6 \times 10^{-19} \text{ J}$$

$$K.E = h\nu - h\nu_0 \text{ (photo-e)} \quad \text{Work fn}$$

$$V = \frac{h\nu}{e} - \frac{h\nu_0}{e}$$

Stopping Potential

$$V = \left(\frac{ke^2}{h}\right) \left(\frac{Z}{n}\right)$$

$$V = 2.18 \times 10^6 \left(\frac{Z}{n}\right) \text{ m/s}$$

$$r = \left(\frac{h^2}{4\pi m k e^2}\right) \left(\frac{n^2}{Z}\right)$$

$$r = 0.529 \left(\frac{Z}{n}\right) \text{ \AA}$$

$$K.E = \frac{1}{2} m \left(\frac{ke^2}{h}\right)^2 \left(\frac{Z^2}{n^2}\right)$$

$$K.E = -13.6 \left(\frac{Z^2}{n^2}\right) \text{ eV/atom}$$

$$= -2.18 \times 10^{-18} \left(\frac{Z^2}{n^2}\right) \text{ J/a}$$

$$= -1312 \left(\frac{Z^2}{n^2}\right) \text{ kJ/mol}$$

$$T \propto \frac{n^3}{Z^2}$$

for H atom)

$$\begin{aligned} K.E_1 &= -13.6 \text{ eV} \\ K.E_2 &= -3.4 \text{ eV} \\ K.E_3 &= -1.5 \text{ eV} \\ K.E_4 &= -0.85 \text{ eV} \end{aligned}$$

Spectral lines

limiting line $\infty \rightarrow n$
 α (or 1st line) $(n+1) \rightarrow n$

Lyman — UV
 Balmer — visible
 Paschen } Infrared
 ...

$n_2 \rightarrow n_1$

$$\Delta E = -13.6 \left[\frac{1}{n_2^2} - \frac{1}{n_1^2} \right] (Z)^2$$

$$\frac{1}{\lambda} = -R_H \left[\frac{1}{n_2^2} - \frac{1}{n_1^2} \right] (Z)^2$$

$$R_H = \frac{1.1 \times 10^7 \text{ m}^{-1}}{\left(\frac{2\pi^2 e^4 \pi m}{h^3 c} \right)}$$

NOTE: $\lambda \propto \frac{1}{\Delta E} \rightarrow$
 $\lambda_{\min}: \infty \rightarrow n$
 $\lambda_{\max}: (n+1) \rightarrow n$

$$\left(\text{Max no. of spectral lines} \right) = (n_2 - n_1) C_2$$

Zelma eff. $\rightarrow B$ (splitting of spectral lines in B field)
 Stark eff. $\rightarrow E$

De-Broglie

$$\lambda_d = \frac{h}{p} = \frac{h}{mv}$$

$h = 6.626 \times 10^{-34} \text{ Js}$

$$\lambda_d = \frac{h}{\sqrt{2mKE}}$$

$$\lambda_d = \frac{h}{\sqrt{2mqV}}$$

for e^- , $\lambda_d = \sqrt{\frac{150}{V}}$ (in \AA)

NOTE: e^- in n^{th} shell makes n waves per circumference

Heisenberg's Uncertainty Principle

$$\Delta x \Delta p \geq \frac{h}{4\pi}$$

$$\Delta x \Delta v \geq \frac{h}{4\pi m}$$

$$\Delta x \Delta \lambda \geq \frac{\lambda^2}{4\pi}$$

$$\Delta E \Delta t \geq \frac{h}{4\pi}$$

$$\Delta (KE) \Delta x \geq \frac{h v}{4\pi}$$

Schrodinger wave Eqn

$$\nabla^2 \psi + 2m \frac{(E - V)^2}{h^2} \psi = 0$$

$$\nabla = \frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} + \frac{\partial^2 \psi}{\partial z^2}$$

$$E\psi = \hat{H}\psi$$

NOTE: Only n, l, m come from SWE

Quantum Nos

$$\text{Orbital angular momentum} = \sqrt{l(l+1)} \hbar$$

$$\text{Spin multiplicity} = 2|S| + 1$$

where $S = \frac{n}{2} \rightarrow$ # unpaired e^-

$$\text{Spin only magnetic moment} = \sqrt{n(n+2)} \text{ B.M}$$

where $\text{B.M} = \frac{e\hbar}{2m} = 9.27 \times 10^{-24}$

NOTE: $l=1 \begin{cases} m=1 (p_x \text{ OR } p_y) \\ m=0 (p_z) \\ m=-1 (p_y \text{ OR } p_x) \end{cases}$

$l=2 \begin{cases} m=-2 (d_{x^2-y^2} \text{ OR } d_{xy}) \\ m=-1 (d_{yz} \text{ OR } d_{zx}) \\ m=0 (d_{z^2}) \end{cases}$

for one e⁻ system,

Energy $\propto n$

for multi e⁻ system,

Energy $\propto (n+l)$

Priority is same if (n+l)

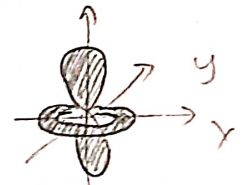
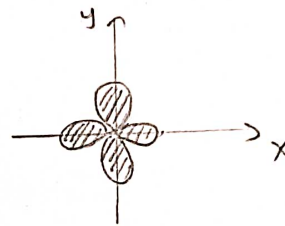
(Spherical/Radial) nodes = $n-l-1$

(Angular nodes) = l

Total nodes = $(n-1)$

$d_{x^2-y^2}$

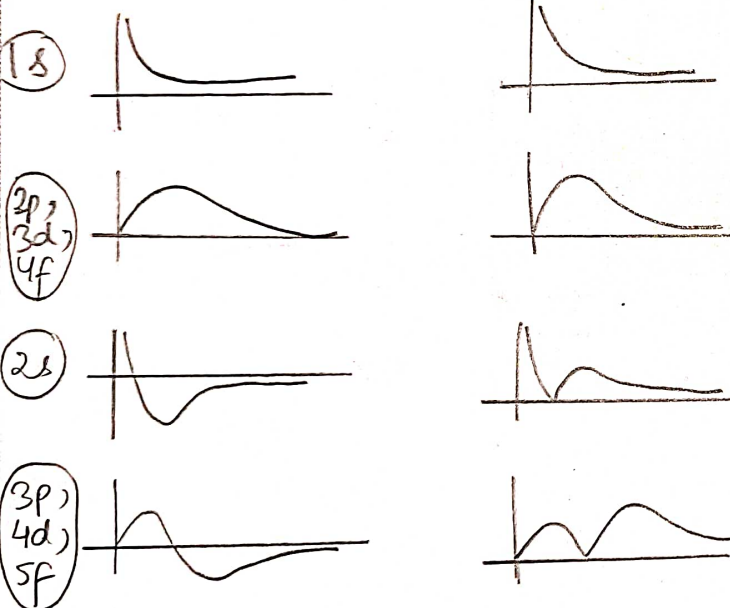
d_{z^2}



Graphs

ψ

ψ^2



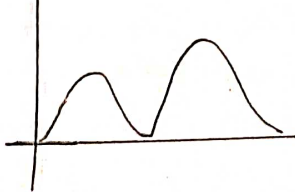
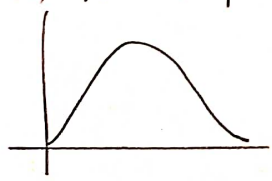
Finding orbital represented by ψ

- ① To find position of Radial Node, find at. which all pts, $\psi^2 = 0 \rightarrow \psi = 0$
- ② Take highest common power of r out of bracket. Its exponent is l
- ③ Highest power of r inside bracket is $(n-l-1)$
- ④ if no θ or $\phi \rightarrow s$ -orbital
if only $\theta \rightarrow$ orbital along z-axis
if both θ & $\phi \rightarrow$ orbital inclined to z-axis

$P = (\psi^2) (4\pi r^2 dr)$

1s, 2p, 3d, 4f

2s, 3p, 4d, 5f



PERIODIC PROPERTIES

(1)

Period	# elements
1	2
2	8
3	8
4	16
5	16
6	32

Atomic Size

$$r_{AB} = r_A + r_B - 0.09 \frac{|\Delta EN|}{\text{Pauling's Scale}}$$

d-block

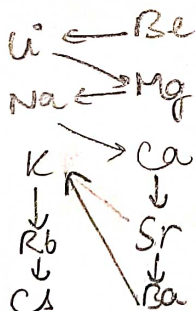
Se < Y < La

RUI for the rest Zn < Cd ~ Hg ~ Uub

p-block

B < Ga < Al < In ~ Te

s-block



F⁻ < Cl⁻ < Br⁻ < I⁻

Ionisation Enthalpy

IE₁ < IE₂ (Successive I.E)

p-block

B > Te > Ga > Al > In

C > Si > Ge > Pb > Sn

d-block

G 7, 8, 9, 11, 12 - 5d > 3d > 4d

G 4, 5, 6, 10 - 5d > 4d > 3d

G 3 - 3d > 4d > 5d

Li < B < Be < C < O < N < F < Cl

Electron-Affinity (EA₂ always < 0)

p-block

Cl > F > Br > I

S > Se > Te > O

P > As > Sb > N (EA < 0 for N-family)

N > C > O > F
P > Si > S > Cl

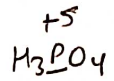
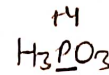
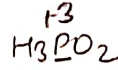
2nd period

Ne < Be < N < B < Li < C < O < F

- $Bi > Pb$

- $I > S$ (highest of G16 < lowest of G17)

- Exception



↑
Most Acidic
(Best Red. Ag.)

Electronegativity

- $F > O > N > Cl > Br > I \sim S \sim C > P \sim H$

- $Ga > Al$

- $Tl > In$

- $Pb > Sn$

Amphoteric Oxides

- $SnO, SnO_2, ZnO, BeO, Al_2O_3, V_2O_3, Sb_2O_3, PbO_2, PbO, MnO, Cr_2O_3, As_2O_3, Cr_2O_3$

Amphoteric Metals - Be, Sn, Ga, Al, Zn, Pb

Neutral Oxides - H_2O, CO, NO, N_2O

1) Pauling's Scale

$$DEN = 0.208 \sqrt{\Delta_{A-B}}$$

$$\Delta_{A-B} = E_{A-B} - \sqrt{E_{A-A} \times E_{B-B}}$$

Resonance energy

2) Mulliken Scale

$$\chi_M = \frac{EA + IE}{2} \text{ (eV/atom)}$$

$$\chi_P = \frac{\chi_M}{2.8}$$

(Pauling)

3) Allred-Rochow

$$\chi_{AR} = 0.359 \frac{Z_{eff}}{r^2} + 0.744$$

$$\text{(\% ionic character)} = 16 (DEN) + 3.5 (DEN)^2$$

Inert Pair Effect

	G13	14	15
PE	Tl^{+3}	Pb^{+4}	Bi^{+5}
	Tl^{+1}	Pb^{+2}	Bi^{+3}

More Stable

p: $\begin{matrix} 2 \\ 3 \end{matrix} \text{] } + (n-2) \text{ more stable}$
 $\begin{matrix} 4 \\ 5 \\ 6 \end{matrix} \text{] } + n \text{ more stable}$

Diagonal Relⁿ

(Metallic radius): $r_{Mg} > r_{Li} > r_{Al}$

(Ionic radius): $r_{Li^+} > r_{Mg^{2+}} > r_{Al^{3+}}$

Uq. Elements - Ga, Br, Fr, Cs, Hg

Metalloids - $At, Te, Sb, Ge, Po, As, Si$

Nature of Ox, HOx, Oxy...

(Acidic strength) \propto (O.S) \propto (E.N.)
Priority

(Basic strength) \propto $\frac{1}{(O.S)}$ \propto $\frac{1}{(E.N.)}$
Priority

Hydration & Lattice Energy

\propto (Charge/Size) \rightarrow Dominant Factor

$$H.E \propto (\text{Hydrated Radii}) \propto \frac{1}{(\text{Mobility})}$$

if $H.E > L.E \rightarrow$ salt is soluble, else insoluble

Thermal Stability

- Mono-anion (F^- , N^{3-} , H^- , O^{2-} , etc)

$$\text{(Thermal Stability)} \propto \text{L.O.E} \propto \left(\frac{\text{Charge}}{\text{Size}}\right)$$

- Poly-anion (CO_3^{2-} , SO_4^{2-} , O_2^{2-} , O_3^{2-} , etc)

$$\text{(Thermal Stability)} \propto \text{(Ionic Char)}$$

Solubility in Water (s-block Elements)

- Solubility of salts decreases down the group.
- Alkali Metals - F^- , OH^- , HCO_3^- , CO_3^{2-} increases down the grp.
- Alkali Earth Metals - F^- , OH^- , HCO_3^- increases down the grp.
 - solubility of Bef_2 is exceptionally high.

EXCEPTIONS

- $Mgf_2 < CaF_2 < SrF_2 < BaF_2 < BeF_2$
- $NaI > LiI > KI > RbI > CsI$
- $LiCl > CsCl > RbCl > NaCl > KCl$

Covalent Bond

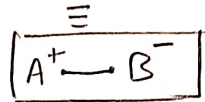
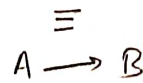
$$\text{(Covalency)} = (\# \text{Covalent Bonds}) + (\# \text{Coordinate Bonds})$$

- * Max covalency of 2nd period elements is 4.

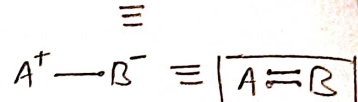
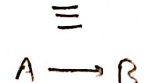
Lewis Octet Theory

Conversion of Coordinate Bond into Simple Covalent

if $A \in 2^{\text{nd}}$ period



if $A \in 3^{\text{rd}}, 4^{\text{th}}$



Resonance

Delocalisation of π -e⁻s.

Happens in conjugated systems, i.e. existence of $(=/\equiv)$, $(=/+)$, $(=/-)$ Backbond in alternate position

$$\text{Bond Order} = \frac{(\# \text{Bond b/w two atoms in all resonating structures})}{(\# \text{Resonating structures})}$$

$$* \text{B.O} = \frac{\sigma + \pi}{\sigma} \text{ b/w two atoms}$$

$$\text{B.O} \propto (\text{Bond strength}) \propto (\text{Bond Energy}) \propto \left(\frac{1}{\text{Bond length}}\right)$$

Valence Bond Theory (VBT)

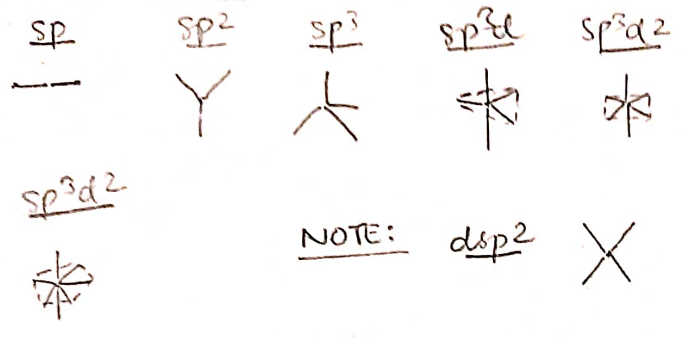
Order of Bond Strength (b/w orbitals)

- $(np - mp) > (np - ms) > (ns - ms)$
 $n \rightarrow$ shell of 1st orb.
 $m \rightarrow$ shell of 2nd orb.

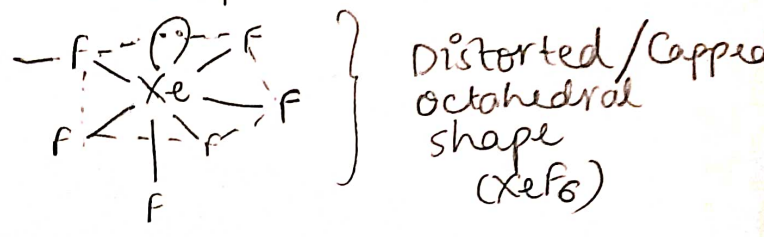
NOTE: shell is dominant factor, so even $(ns - ns) > (n+1)p - (n+1)p$

- $(d\pi - d\pi) > (d\pi - p\pi) > (p\pi - p\pi)$

Hybridisation



- $SCl_6, SBr_6, SI_6 \rightarrow$ do not exist
- XX'_2 do not exist (where $X' > X$)
Interhalogen comp.



VSEPR

Order of Repulsion

- $(lp-lp) > (lp-bp) > (bp-bp)$
- $(\text{Multiple bond} - Mb) > (Mb - Sb) > (\text{Single Bond} - Sb)$

Bent's Rule

- sp^3d : More E.N. atom \rightarrow Axial position
 $l.p. \rightarrow$ Eq. position
- sp^3d^3 : More E.N. atom \rightarrow Eq. post.
 $l.p. \rightarrow$ Ax. post.

NOTE: $\theta \propto (\% s\text{-char}) \propto (E.N. \text{ of central atom}) \propto \frac{1}{(\text{Bond length})}$

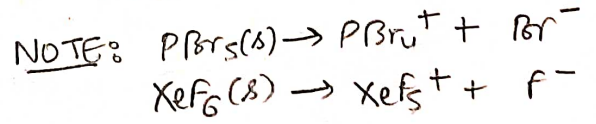
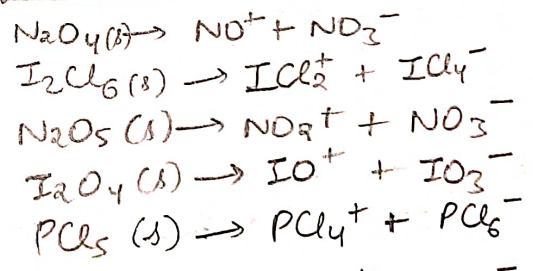
(\angle b/w bonds)

- NOTE:
- In PF_5 , due to berry pseudorotation all bond lengths/energies are equal.
 - SF_6 is inert
-

Hybⁿ in odd e⁻ species

- If side atom of High E.N. (F, O, N, Cl), then unpaired e⁻ included in hyb^n .
- If l.p. & unpaired e⁻ both present, unp. e⁻ NOT included.

Hybⁿ in solid Compounds



Drago's Rule

- No hyb^n when $\text{stearic no.} = 4$ & central atom has 1 l.p.
 - Central atom E 3rd or Higher Period
- | | | |
|---------|---------|-------|
| PH_3 | H_2S | HCl |
| AsH_3 | H_2Se | HBr |
| SbH_3 | H_2Te | HI |

$(E.N. \text{ of side atom}) < 2.5$

Bond Angle

- Priority-wise:
- Hybn of central atom (Direct prop.)
 - # l.o.p (Indirect prop.)
 - E.N of
 - Central Atom (Direct)
 - Side Atom (Indirect)

NOTE: if Bulky side atom/group,
E.N does NOT matter.
(eg - CCl_3 , CH_3^- , ...)

[Bond order, Bond Energy & Bond length have been covered under Resonance]

Bonding in e⁻-Deficient Species

Back Bonding

- Condⁿ:-
- one atom must have l.o.p & other a vacant orbital
 - One of the bonded atoms (A or B) should be of 2nd period. Other one can be of 2nd or 3rd period.

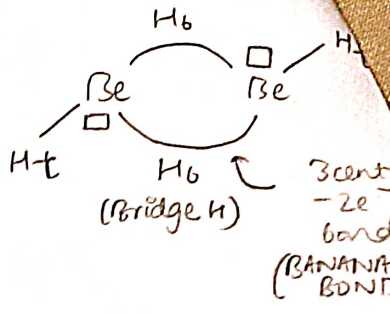
NOTE: Hybn of central atom changes when it donates a l.o.p to form a back bond.

sub NOTE: if side atom is Cl, Br, I, then hybn does NOT change.

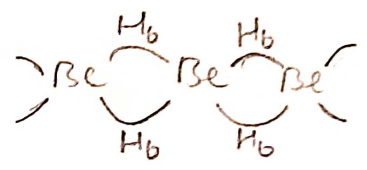
NOTE: Max. 1 back-bond is formed by any atom with another atom.

Bridge Bonding

- Be
- BeF_2 X No dimer (strong Back Bond)
 - BeH_2
 - gas



- solid

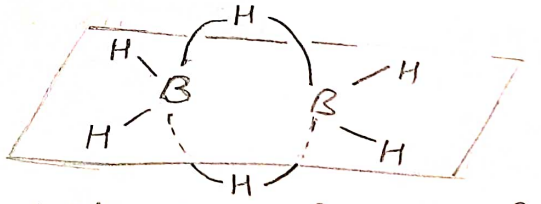


NOTE: Bond length ($Be-H_b$) > Bond length ($Be-H_t$)

- B
- BF_3 X No dimer (strong Back Bond)
 - BCl_3 , BBr_3 , BI_3 X No dimer (High steric Crowding)

- BH_3 Dimer Polymer X (only 1 vacant orbital)

NOTE:



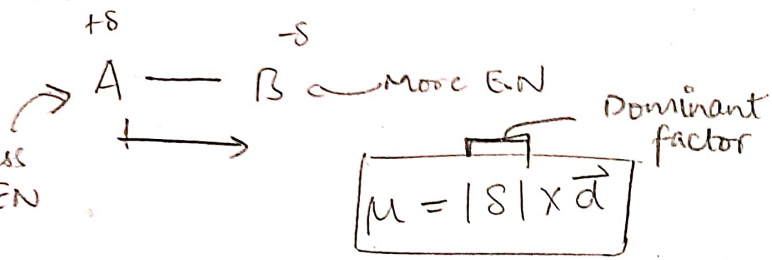
Bridge bond is above & below the plane

- Al
- AlF_3 X No dimer (Predominant ionic)
 - $AlCl_3$, AlH_3 , $Al(C_2H_5)_3$
 - Dimer in vapour
 - Polymer in solid

- $AlBr_3$, AlI_3 Dimer Polymer X (steric Crowding)

Dipole Moment (μ)

(Ionic char in Cov. compound)



$1D = 10^{-18}$ esu cm
 $1D = 3.3 \times 10^{-30}$ Cm

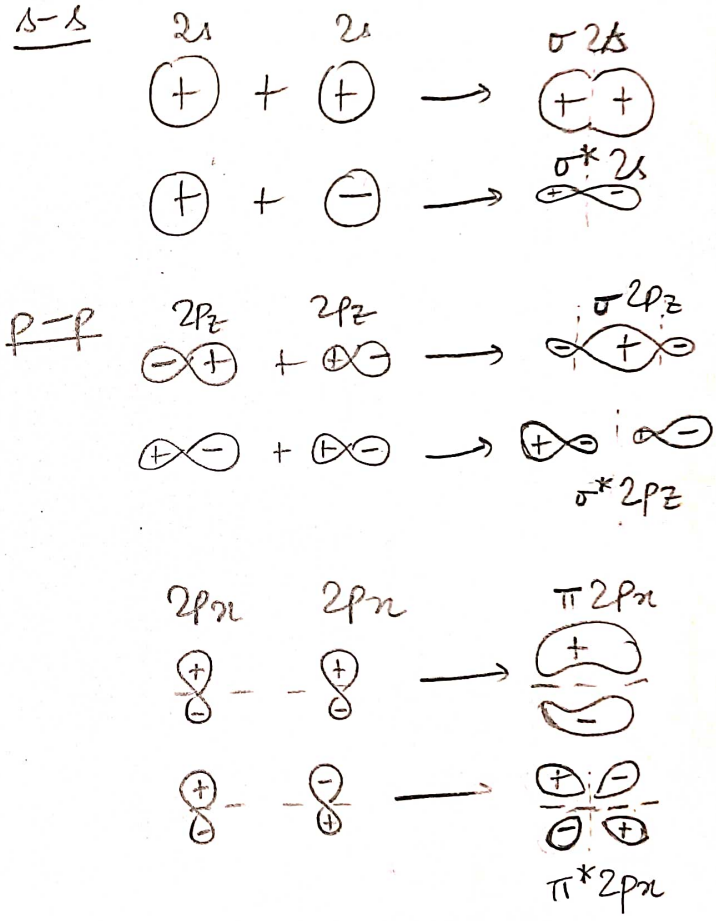
$e \begin{cases} 4.8 \times 10^{-10} \text{ esu} \\ 1.6 \times 10^{-19} \text{ C} \end{cases}$

- $\text{NH}_3 > \text{NF}_3$
- $\text{CH}_3\text{Cl} > \text{CH}_3\text{F} > \text{CH}_3\text{Br} > \text{CH}_3\text{I}$
- $\text{CH}_2\text{F}_2 > \text{CH}_2\text{Cl}_2 > \text{CH}_2\text{Br}_2 > \text{CH}_2\text{I}_2$
 $\text{F} : [2 > 1 > 3]$
- $\text{CH}_3\text{X} > \text{CH}_2\text{X}_2 > \text{CHX}_3 > \text{CH}_4/\text{CX}_4$
 $\text{X} : [1 > 2 > 3]$
 $\{X = \text{Cl}, \text{Br}, \text{I}\}$

$(\% \text{ ionic char}) = \frac{|\delta|}{|e|} \times 100\%$

Molecular Orbital Theory

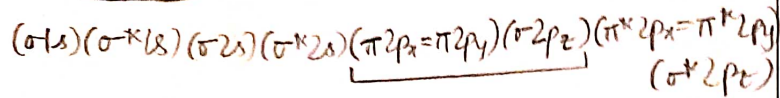
(Gerade orbitals) - orbitals which remain same after rotating 180° abt 2 axis subsequently



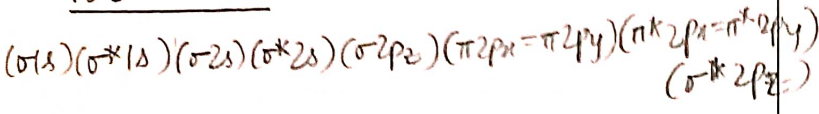
NOTE: Gerade - σ, π^*
 ungerade - σ^*, π

e⁻ Config

upto 14e



15e⁻ to 20e⁻



B.O

e ⁻	B.O
12	2
13	2.5
14	3
15	2.5
16	2

$$B.O = \frac{1}{2} [N_b - N_a]$$

e⁻ in ABMO

e⁻ in BMO

if Unpaired e⁻ - Paramagnetic

EXCEPTIONS

- CO : $(\sigma 1s^2)(\sigma 2p_z^2)(\pi 2p_x^2 = \pi 2p_y^2)(\sigma^* 2s^2)$
 $B.O(CO) = 3$
 $B.O(CO^+) = 3.5$

- Halogens show color despite being diamagnetic

- F₂ → pale yellow
- Cl₂ → light green
- Br₂ → brown
- I₂ → violet

Reason: Diff. b/w HOMO & LUMO is NOT too great.

HOMO - Highest occupied MO
LUMO - lowest unoccupied MO

Unit Conversions

Temperature -

$$\frac{C-0}{100-0} = \frac{K-273}{373-273} = \frac{F-32}{212-32}$$

Volume -

$$\begin{aligned} 1\text{m}^3 &= 1000\text{L} \\ 1\text{dm}^3 &= 1\text{L} \\ 1\text{cm}^3 &= 1\text{ml} \end{aligned}$$

Pressure -

$$1\text{atm} = 760\text{ mmHg} = 76\text{ cm Hg} \\ = 760\text{ torr}$$

$$1\text{atm} = 1.01\text{ bar} = 1.013 \times 10^5\text{ Pa}$$

$$\left(\text{Pressure at } t^\circ\text{C} \right) = P_0 + \frac{t}{273} P_0$$

$P_0 \rightarrow$ Pressure at 0°C

Avogadro's Law -

$$\frac{V}{n} = \text{const.}$$

given P, T const.

Ideal Gas Eqn

$$PV = nRT$$

$$R = 0.0821 \frac{\text{atmL}}{\text{molK}} \left(\text{use } \frac{25}{300} \right)$$

$$= 8.314 \frac{\text{J}}{\text{molK}} \left(\text{use } \frac{25}{3} \right)$$

$$= 2 \frac{\text{cal}}{\text{molK}}$$

Gas Laws

Boyle's Law - $PV = \text{const.}$
given T const.

Charles' Law - $\frac{V}{T} = \text{const.}$
given P const.

$$\left(\text{Vol. at } t^\circ\text{C} \right) = V_0 + \frac{t}{273} V_0$$

$V_0 \rightarrow$ Vol. at 0°C

Gay Lussac's Law - $\frac{P}{T} = \text{const.}$

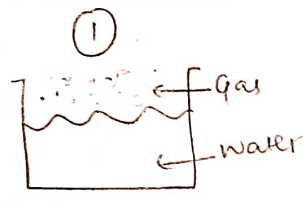
Dalton's Law of Partial Pressures

(only applicable for non-reacting gases)

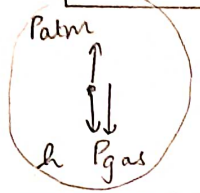
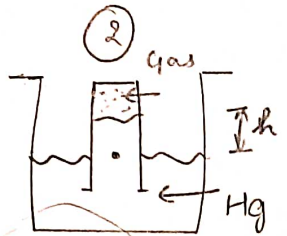
$$P_{\text{gas}} = X_{\text{gas}} \cdot P_{\text{Total}}$$

\therefore Each gas is assumed to occupy the whole volume.

Configurations (FBD of liq. column)

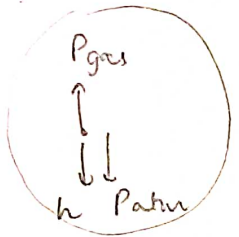
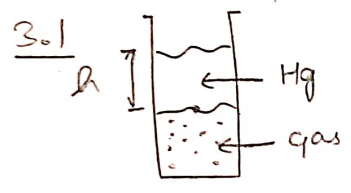


$$P_{wet\ gas} = P_{gas} + (\text{Vapour Pressure})$$



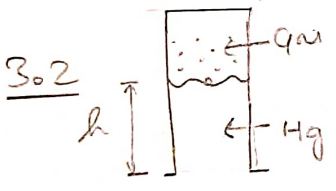
$$P_{atm} = P_{gas} + h \text{ mm Hg}$$

3



$$P_{gas} = (P_{atm} + h) \text{ mm Hg}$$

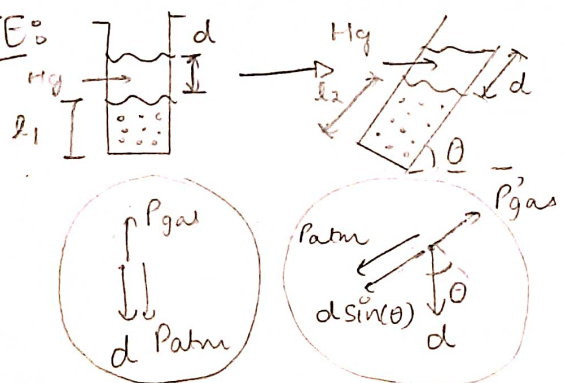
760



$$P_{atm} = P_{gas} + h$$

76 mm Hg

NOTE:

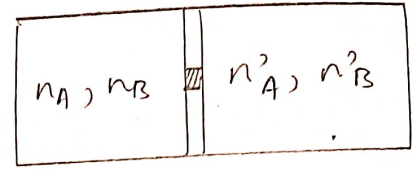


$$P_g V = P_g' V'$$

$$\Rightarrow (P_{atm} + \rho g d) l_1 = (P_{atm} + \rho g d \sin(\theta)) l_2$$

$$\Rightarrow (P_{atm} + \rho g d) l_1 = (P_{atm} + \rho g d \sin(\theta)) l_2$$

Graham's Law of Diffusion



$$\frac{x_A}{x_B} = \frac{P_A}{P_B} \sqrt{\frac{M_B}{M_A}}$$

NOTE:

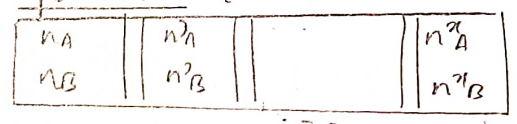
$$\frac{P_A}{P_B} = \frac{n_A}{n_B} = \frac{x_A}{x_B} = \frac{w_A \cdot M_B}{w_B \cdot M_A}$$

$$\frac{n'_A / l_A}{n'_B / l_B} = \frac{n_A}{n_B} \sqrt{\frac{M_B}{M_A}}$$

if $l_A = l_B$,

$$\frac{n'_A}{n'_B} = \frac{n_A}{n_B} \sqrt{\frac{M_B}{M_A}}$$

Enrichment/ Separation factor



n → # steps

$$\frac{n^1_A}{n^1_B} = \frac{n_A}{n_B} \left(\frac{M_B}{M_A} \right)^{n/2}$$

Enrichment/ Separation Factor

Rate of effusion $\propto \frac{PA}{\sqrt{2\pi MRT}}$

A → cross-sectional area of orifice

Kinetic Theory of Gases

• Kinetic Eqn of Gas

$$PV = \frac{1}{3} mN V_{rms}^2$$

$m \rightarrow$ wt. of one molecule
 $N \rightarrow$ # Molecules
 $V_{rms} \rightarrow$ Rt. mean sq. velocity

• Kinetic energy

- n mol : $\frac{3}{2} nRT$
 - 1 molecule : $\frac{3}{2} k_b T$

(Boltzman Const.)
 $k_b = \frac{R}{N_A}$
 $= 1.38 \times 10^{-23} \frac{J}{K}$

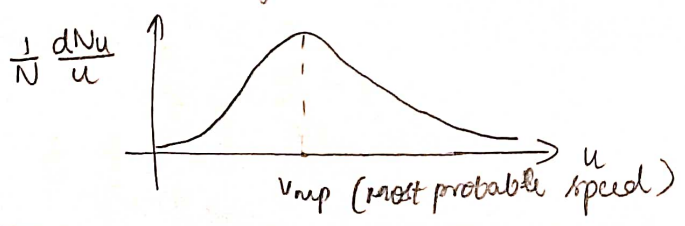
• Density of Gas

$$d = \frac{PM}{RT}$$

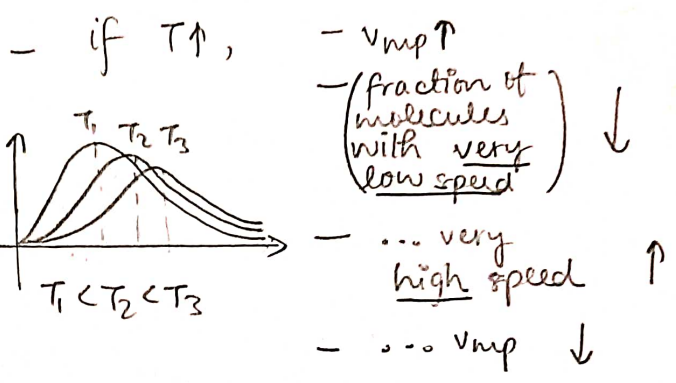
Maxwell Dist. of Molecular speeds

$$dNu = 4\pi N \left(\frac{M}{2\pi RT}\right)^{3/2} e^{-\frac{Mu^2}{2RT}} u^2 du$$

$N \rightarrow$ # gas molecules
 $Nu \rightarrow$ # molecules having velocity in range u to $(u+du)$



NOTE: - Area under curve $\left(\frac{1}{N} \frac{dNu}{du} \text{ vs } u\right)$ is 1.



- Graphs same when v_{mp} same

Molecular Speeds


- Most probable : $\sqrt{\frac{2RT}{M}}$
- Average : $\sqrt{\frac{3RT}{\pi M}}$
- Rt. mean sq. : $\sqrt{\frac{3RT}{M}}$

NOTE: $v_{mp} < v_{avg} < v_{rms}$

Maxwell Distribution of Kinetic Energy

$$dNE = 2\pi N \left(\frac{1}{\pi RT}\right)^{3/2} e^{-\frac{E}{RT}} \sqrt{E} dE$$

- Most probable Kinetic Energy (E_{mp}) - $\frac{1}{2} RT$

Collision freq. (Z_{11})  $N^* = \frac{N}{V}$

$Z_1 = (\pi \sigma^2) (\sqrt{2} v_{avg}) (N^*)$

(Collisions b/w a molecule with other molecules per unit time)

$Z_{11} = Z_1 \left(\frac{N^*}{2}\right)$

(Total collisions b/w the similar molecules per unit time per unit time) $\frac{1}{2} \pi \sigma^2 v_{avg} (N^*)^2$

$N^* \propto \frac{P}{T}$

$Z_{11} \propto \frac{P^2}{T^{3/2}}$

- At $P = \text{const.}$
 $Z_{11} \propto \frac{1}{T^{3/2}}$

- At $T = \text{const.}$
 $Z_{11} \propto P^2$

- At $V = \text{const.}$ (rigid container)
 $\frac{P}{T} = \text{const.}$
 $\Rightarrow Z_{11} \propto \sqrt{T}$

Mean Free Path (λ)

Avg. dist. travelled by a gas molecule b/w two successive collisions

$\lambda = \frac{1}{\sqrt{2} \pi \sigma^2 N^*}$

$\lambda \propto \frac{T}{P}$

- At $P = \text{const.}$ $\lambda \propto T$

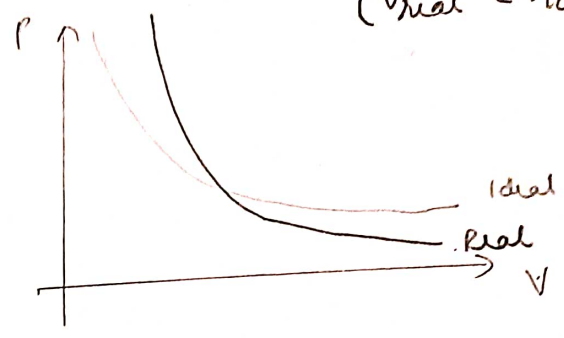
- At $T = \text{const.}$ $\lambda \propto \frac{1}{P}$

- At $V = \text{const.}$ (rigid container) $\lambda = \text{const}$ [$\because P/T = \text{const.}$]

Real Gas

High $P \rightarrow$ significant deviation ($V_{real} > V_{ideal}$)

low P & High $T \rightarrow$ Behaviour closer to ideal gas ($V_{real} < V_{ideal}$)



Volume Correction
 $V_{ideal} = V_{real} - \text{Correction}$
 $= V_{real} - nb$

$b \rightarrow$ excluded vol. for 1 mol gas molecules (extended vol. or co-volume)

$b = 4 \times (\text{vol. of 1 mol gas molecules})$

Pressure Correction
- depends on force & freq. of collision

$P_{real} = P_{ideal} - \text{Correction}$
 $= P_{ideal} - \frac{an^2}{V^2}$

(Excluded volume for one gas molecule) $= 4 \times \left(\frac{4}{3} \pi r^3\right)$

Vander Wall's Eqn

$\left(P + \frac{an^2}{V^2}\right) (V - nb) = nRT$

NOTE: NOT applicable to H_2 & He as only repulsive forces exist b/w molecules of these gas; which are not considered while calculating corrections.

Compressibility factor:

$$Z = \frac{V_{real}}{V_{ideal}} \quad (V_m = \frac{V}{n})$$

$$\Rightarrow Z = \frac{P_{ideal} V_{real}}{nRT} = \frac{P V_m}{RT}$$

NOTE: - if $Z=1$, gas is ideal

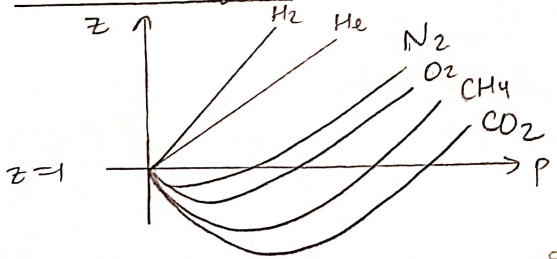
- if $Z < 1 \Rightarrow V_R < V_i$

- -ve deviation
- attractive forces dominant
- low Pressure
- can be compressed (liquefied)

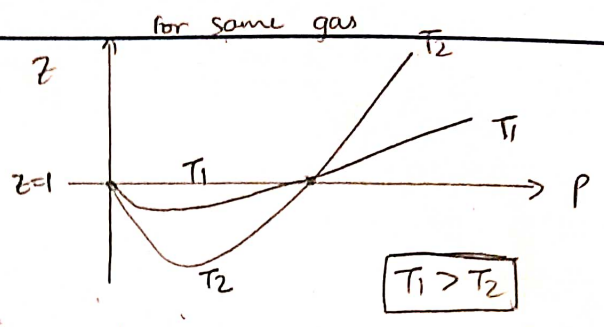
- if $Z > 1 \Rightarrow V_R > V_i$

- +ve deviation
- repulsive forces dominant
- High P
- Difficult to compress

Variation of Z



NOTE: Lower the dip, easier it is to liquefy gas.



Z under diff. condⁿs

① low P $(V-nb) \sim V$
 $(P + \frac{a}{V_m^2})(V_m) = RT$
 $\Rightarrow Z = 1 - \frac{a}{V_m RT}$

② low P & High T $(P + \frac{an^2}{V^2}) \sim P$
 $P V_m = RT$ $(V-nb) \sim V$
 $\Rightarrow Z = 1$

③ High P $(P + \frac{an^2}{V^2}) \sim P$
 $P(V-nb) = RT$
 $\Rightarrow Z = 1 + \frac{Pb}{RT}$

Misc. Pts.

① Second virial coeff - $(b - \frac{a}{RT})$
 third virial coeff. - b^2

② Critical constants

R.T.O -

-(P_c) - Min. P req. to cause liq. at T_c.

$$P_c = \frac{a}{27b^2}$$

-(V_c) - volume occupied by one mol. gas at P_c & T_c.

$$V_c = 3b$$

-(T_c) - Max T at which a gas can be liquified.

$$T_c = \frac{8a}{27Rb} = \frac{8T_b}{27}$$

3) Boyle Temp. (T_b):
T at which gas behaves as ideal gas for a defined range of low pressure

$$T_b = \frac{a}{Rb}$$

4) Inversion Temp. (T_i):
T at which gas shows no Joule-Thompson effect

$$T_i = \frac{2a}{Rb} = 2T_b$$

NOTE:

Joule-Thompson effect $\left\{ \begin{array}{l} \text{all gases except H}_2 \text{ \& He} \\ \text{- cooling effect} \\ \text{H}_2 \text{ \& He - heating effect} \end{array} \right.$

Eudiometry

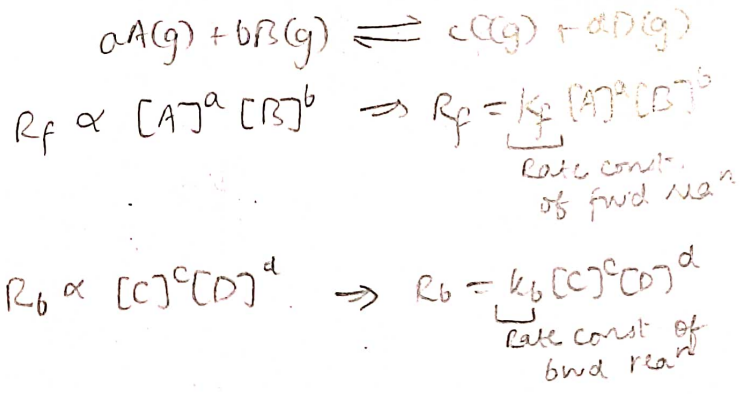
Absorbant	Gas Absorbed
- NaOH/KOH sol ⁿ	CO ₂ , SO ₂ , NO ₂ , Halogens
- Ammonical CuCl ₂	CO, C ₂ H ₂
- Turpentine oil	O ₃
- Alkaline Pyrogallol	O ₂
- Conc. H ₂ SO ₄	Moisture, NH ₃
- FeSO ₄ sol ⁿ	NO
- Heated Mg	N ₂

6

Active Mass

- for liq. (Active Mass) = (Molar conc.)
- for gases (Active Mass) $\begin{cases} \text{(Molar conc.)} \\ \text{(Partial P)} \end{cases}$
- for solids & liq. medium in which the rxn is taking place
 $\left[\because \text{density} = \text{const.} \right]$ (Active Mass) = const. [assumed to be 1]
- (Active mass) = $\frac{\text{mol.}}{\text{vol.}} = \frac{w}{M \times V} = \frac{\text{density}}{\text{Molar Mass}}$

Law of Mass Action



NOTE: Rate const. (k) depends only on Temperature & Catalyst.

Law of Chemical Eq.

At eq. $R_f = R_b$ (condⁿ for eq)

$$\Rightarrow k_f [A]^a [B]^b = k_b [C]^c [D]^d$$

$$\Rightarrow \left(\frac{k_f}{k_b} \right) = \frac{[C]^c [D]^d}{[A]^a [B]^b}$$

$$\Rightarrow K_{eq} = \frac{[C]^c [D]^d}{[A]^a [B]^b}$$

$$K_c = \frac{[C]^c [D]^d}{[A]^a [B]^b}$$

units: $\left(\frac{\text{mol}}{L} \right)^{\Delta n_g}$

$$K_p = \frac{(P_C)^c (P_D)^d}{(P_A)^a (P_B)^b}$$

units: $(\text{atm})^{\Delta n_g}$

$$K_x = \frac{(X_C)^c (X_D)^d}{(X_A)^a (X_B)^b}$$

unitless

NOTE: - defn & value of K_{eq} only holds at eq.

- K_{eq} is fixed for a given T i.e. it is T dependent
- K_{eq} is independent of conc., pressure, volume, catalyst, etc.

★ When aq. species (solute/ion) & gaseous substance are present together,
 eg: $NH_3(g) + H_2O(l) \rightleftharpoons NH_4^+(aq) + OH^-(aq)$

$$K_{pc} = \frac{[NH_4^+][OH^-]}{P_{NH_3}}$$

(Partial P) \rightarrow ↑ (of gas) (conc. of aq. species)

Relⁿ b/w (K_p & K_c) & (K_p & K_x)

- $K_p = K_c (RT)^{\Delta n_g}$
- $K_p = K_x (P_{Total})^{\Delta n_g}$

NOTE: $K_p = K_c \forall \Delta n_g$, when

$$T = \frac{1}{R} \sim 12K$$

Factors Affecting K_{eq}

① Mode of Repⁿ & Stoichiometry of Reaⁿ

If K_{eq} of $aA(g) + bB(g) \rightleftharpoons cC(g) + dD(g)$

is K, then

- $cC(g) + dD(g) \rightleftharpoons aA(g) + bB(g)$; $\left(\frac{1}{K}\right)$

- $2aA(g) + 2bB(g) \rightleftharpoons 2cC(g) + 2dD(g)$; (K^2)

- $\frac{a}{2}A(g) + \frac{b}{2}B(g) \rightleftharpoons \frac{c}{2}C(g) + \frac{d}{2}D(g)$; (\sqrt{K})

- If rean^s with K_{eq} = K₁ & K₂ respectively are added (or subtracted) the K_{eq} of resulting reanⁿ will be $(K_1 K_2)$ (or (K_1 / K_2))

② Effect of Temp.

$$\log(K_{eq}) = \frac{\Delta S}{2.303R} - \frac{\Delta H}{2.303RT}$$

$\Delta S \rightarrow$ Entropy change
 $\Delta H \rightarrow$ Enthalpy change

$$\log\left(\frac{K_2}{K_1}\right) = \frac{\Delta H}{2.303R} \left[\frac{1}{T_1} - \frac{1}{T_2}\right]$$

NOTE: When T \uparrow , reanⁿ moves in Endothermic dirxn. ($\Delta H > 0$)

Similarly, when T \downarrow \rightarrow Exothermic dirxn ($\Delta H < 0$)

Reaⁿ Quotient

$$Q = \frac{[C]^c [D]^d}{[A]^a [B]^b} \text{ at ANY inst.}$$

At eq, $Q = K_{eq}$

if $Q > K_{eq} \rightarrow$ Reaⁿ moves Back

if $Q < K_{eq} \rightarrow$ Reaⁿ moves Forw

Le Chatelier's Principle

Reaⁿ shifts in a dirxn so as to nullify effect of change

• Conc.: $A(g) \rightleftharpoons B(g)$

if [A] $\downarrow \rightarrow$ Reaⁿ moves back

if [A] $\uparrow \rightarrow$ Reaⁿ moves forw

• Pressure: if P $\uparrow \rightarrow$ Reaⁿ will move in dirxn where less # gaseous moles formed

NOTE: if $\Delta n_g = 0$, no change takes place

• Volume: if V $\uparrow \rightarrow$ Reaⁿ will move in dirxn where more # gaseous moles formed

• Addⁿ of Inert Gas

① At V=const., No change

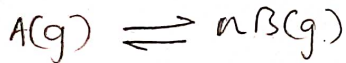
② At P=const., towards more # gaseous moles
(Inert gas \nrightarrow V \uparrow) \Rightarrow # gaseous moles

NOTE: Addⁿ or removal of solid results in no change.

(Regardless of whether it is inert or a reactant/product)

Degree of Dissociation & Vapour Density

$\alpha \rightarrow$ # mol. dissociated per mole of a particular specie



$$n_i: a \quad 0$$

$$n_f: a(1-\alpha) \quad na\alpha$$

$D \rightarrow$ Theoretical V.D.

$d \rightarrow$ observed V.D

By Conservation of Mass,

$$w_i = w_f$$

$$\Rightarrow M_i n_i = M_f n_f$$

$$\Rightarrow \frac{M_i}{M_f} = \frac{D}{d} = \frac{n_f}{n_i} = \frac{a(1-\alpha) + na\alpha}{a}$$

$$\Rightarrow \boxed{\frac{M_i}{M_f} = \frac{D}{d} = \frac{1+(n-1)\alpha}{1}}$$

$$\boxed{\alpha = \frac{D-d}{(n-1)d}}$$

(Remember the process, not the formula!)

Physical Eq.



$T \uparrow \Rightarrow$ fwd rea^n

$P \uparrow \Rightarrow$ brwd rea^n



$T \uparrow \Rightarrow$ fwd rea^n

★ Vol. of $H_2O(s) >$ Vol. of $H_2O(l)$

$P \uparrow \Rightarrow$ rea^n moves to $V \downarrow$

\downarrow
fwd (liq. side)

NOTE: This is true for most solids, i.e. their vol. is greater than their liq. form.



- $\Delta H > 0$

- Graphite $\begin{matrix} \uparrow \text{ More Volume} \\ \downarrow \text{ Less Energy} \end{matrix}$

- Diamond $\begin{matrix} \uparrow \text{ Less Volume} \\ \downarrow \text{ More Energy} \end{matrix}$

So $T \uparrow \Rightarrow$ fwd rea^n

$P \uparrow \Rightarrow V \downarrow \Rightarrow$ fwd rea^n

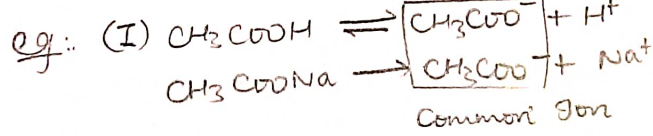
EQUILIBRIUM

Factors affecting Degree of Dissoc.

- 1) Nature of Electrolyte - $\alpha \sim 1 \Rightarrow$ strong
 $\alpha \ll 1 \Rightarrow$ weak
- 2) Temp - $\alpha \propto \text{Temp.}$
as $\Delta H > 0$ for dissoc. reⁿs.
- 3) Dilution - $\text{Dil} \uparrow \Rightarrow \alpha \uparrow$
as $K_{eq} = \alpha^2$ & $\alpha \propto \frac{1}{V}$ and $\text{Dil} \Rightarrow V \uparrow$

Common Ion Effect

Suppression of DoD of weak electrolyte in presence of strong electrolyte having common ion.



\Rightarrow DoD of reⁿ (I) \downarrow

Acid-Base Theories

- | | | |
|----------------------------|--|---|
| | <u>Acid</u> | <u>Base</u> |
| 1) <u>Arrhenius</u> - | give H^+
in aq. sol ⁿ | give OH^-
in aq. sol ⁿ |
| 2) <u>Bronsted Lowry</u> - | give H^+ | take H^+ |
| 3) <u>Lewis</u> - | take l.p.
(Electrophiles) | give l.p.
(Nucleophiles) |

NOTE:

<u>Electrolyte</u>	<u>Conj. base/acid</u>
Strong	Weak
Weak	Strong

Weak Monocacidic Bases & Monobasic Acids.

- 1) Acids
 $\alpha = \sqrt{\frac{K_a}{C}}$ $[\text{H}^+] = \alpha C = \sqrt{K_a C}$
 $\text{pH} = \frac{1}{2} (\text{p}K_a - \log(C))$
- 2) Bases
 $\alpha = \sqrt{\frac{K_b}{C}}$ $[\text{OH}^-] = \alpha C = \sqrt{K_b C}$
 $\text{pOH} = \frac{1}{2} (\text{p}K_b - \log(C))$

NOTE: These formulae only work if $\alpha < 0.02 \text{ M}$.
 Else, $K = \frac{\alpha^2}{(1-\alpha)}$ & $[\text{H}^+] = \alpha$ (or $[\text{OH}^-] = \alpha$)

Mixing of Weak Acids & Weak Bases

Let us take V_1 of M_1 mol/L HA_1 (or B_1OH) & V_2 of M_2 mol/L HA_2 (or B_2OH).

$$M_{\text{net}} = \sqrt{K_1 C_1 + K_2 C_2}$$

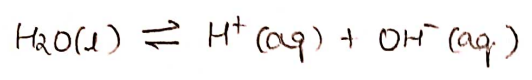
	<u>Acids</u>	<u>Bases</u>
$C_1 = \frac{M_1 V_1}{M_1 V_1 + M_2 V_2}$	$K_1 = K_{a1}$	K_{b1}
$C_2 = \frac{M_2 V_2}{M_1 V_1 + M_2 V_2}$	$K_2 = K_{a2}$	K_{b2}

Self-dissoc. of water

1) For pure water $[H_2O] = 55.5 \text{ mol/L}$.

$$M = \frac{W_{\text{solute}}}{V_{\text{solvent}}} = \frac{n_{H_2O}}{V_{H_2O}} = \frac{1000g}{18g/mol} \times \frac{1}{1L}$$

(H_2O is both solute & solvent here) = 55.5 mol/L



$$K_{eq} = \frac{[H^+][OH^-]}{[H_2O]} = \frac{[H^+][OH^-]}{55.5}$$

$$\Rightarrow [H^+][OH^-] = K_w \quad \& \quad K_w = 55.5 K_{eq}$$

Ionic product of water.

@ $T = 25^\circ C$, $K_w = 10^{-14}$

NOTE: (i) for pure water at any T,
 $[H^+] = [OH^-] = \sqrt{K_w} = 10^{-7} @ 25^\circ C$

(ii) $pH + pOH = pK_w = 14 @ 25^\circ C$

(iii) $T \uparrow \Rightarrow K_w \uparrow \Rightarrow pH \downarrow$

2) $K_a K_b = K_w$
 electrolyte conjugate

NOTE: While calculating pH of extremely dil. solns of strong electrolytes, we also take into account the $[H^+]$ & $[OH^-]$ furnished by $[H_2O]$ itself.

eg. 10^{-8} M HCl
 $[H^+] = 10^{-8} + 10^{-7}$ (by water)
 $= 11 \times 10^{-8}$

$pH = 8 - \log(11) = 6.9$

Salt Hydrolysis

1) SA+SB salt - Salt does NOT hydrolyse

2) SA+WB salt -

$$K_h = \frac{K_w}{K_b} \quad h = \sqrt{\frac{K_w}{K_b C}}$$

$$pH = 7 - \frac{1}{2} [pK_b + \log(C)]$$

3) WA+SB salt -

$$K_h = \frac{K_w}{K_a} \quad h = \sqrt{\frac{K_w}{K_a C}}$$

$$pH = 7 + \frac{1}{2} [pK_a + \log(C)]$$

4) WA+WB Salt -

$$K_h = \frac{K_w}{K_a K_b} \quad h = \sqrt{\frac{K_w}{K_a K_b}}$$

$$pH = 7 + \frac{1}{2} [pK_a - pK_b]$$

5) Amphiprotic / Amphoterics Salts -

For $M_x H_{(n-x)} A$ salt of $H_n A$ acid,

$$pH = \frac{1}{2} [pK_{a1} + pK_{a2}]$$

Buffer Soln

1) Mix Buffer

- 1.1) Acidic Buffer -
 - 1.1.1) Weak Acid + (its strong basic salt)
 - 1.1.2) Weak Acid + (its conj base)

- 1.2) Basic Buffer -
 - 1.2.1) Weak Base + (its strong acidic salt)
 - 1.2.2) Weak Base + (its conj acid)

2) Simple Buffer

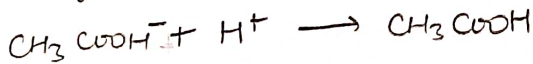
2.1) Salt of weak Acid & weak Base

ACIDIC BUFFER

$$pH = pK_a + \log\left(\frac{[Conj. Base]}{[Acid]}\right)$$

Buffer Action:

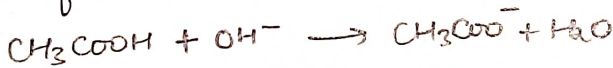
i) Addn of H^+ -



$[i]:$	S	x	a
$[f]:$	S-x	0	a+x

$$pH = pK_a + \log\left(\frac{S-x}{a+x}\right)$$

ii) Addn of OH^- -



$[i]:$	a	x	S
$[f]:$	a-x	0	S+x

$$pH = pK_a + \log\left(\frac{S+x}{a-x}\right)$$

BASIC BUFFER

$$pOH = pK_b + \log\left(\frac{[Conj. Acid]}{[Base]}\right)$$

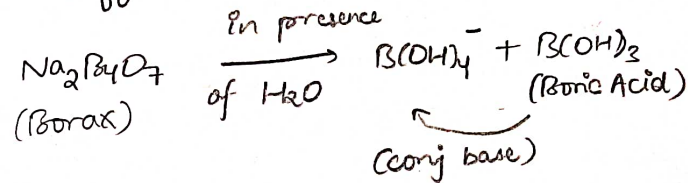
NOTE: 1) For effective buffer

Acidic
 $0.1 \leq S/a \leq 10$
 $\Rightarrow pH = pK_a \pm 1$

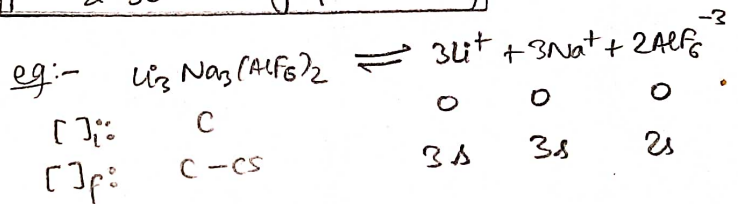
Basic
 $0.1 \leq S/b \leq 10$
 $pOH = pK_b \pm 1$

$$2) \text{ Buffer capacity} = \frac{\text{Change in mols of } H^+/OH^- \text{ per L}}{\Delta pH}$$

3) 'Boric Acid + Borax' is a buffer.



Solubility & solubility product



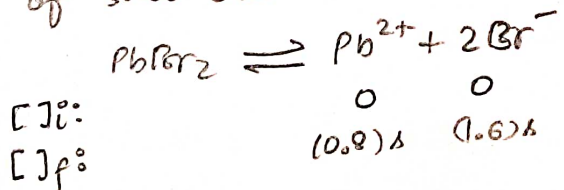
$$K_{sp} = [Li^+]^2 [Na^+]^3 [AlF_6^{3-}]^2$$

$$= (3s)^2 (3s)^3 (2s)^2$$

$$= 3^6 2^2 s^8$$

Q. At 25°C, K_{sp} for $PbBr_2$ is 8×10^{-5} . If salt is 80% dissociated, what is solubility of $PbBr_2$?

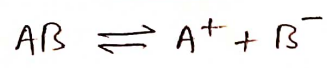
A) $S = \text{Max. \# mol. dissolved.}$
In this case $(0.8)s$ mol. of salt dissolves.



$$K_{sp} = [0.8s][1.6s]^2 = 8 \times 10^{-5}$$

$$\Rightarrow s = \sqrt[3]{\frac{10^{-4}}{2.56}}$$

Precipitate formation



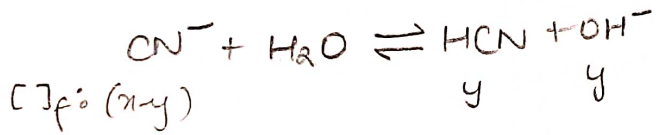
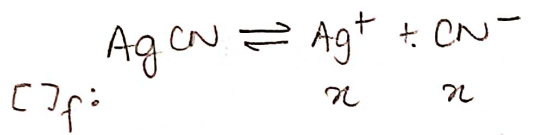
$$Q = [A^+][B^-] \text{ at any pt. of time.}$$

↑
Ionic prod.

- $Q < K_{sp}$: ppt NOT form
- $Q = K_{sp}$: Eq. condⁿ
- $Q > K_{sp}$: ppt will form

Solubility of AgCN

CN⁻ being conj base of HCN (weak acid) it hydrolyses



At eq. [CN⁻] = (x-y)
 [HCN] = y

$$K_{sp} = [Ag^+][CN^-] = x(x-y)$$

$$K_h = \frac{y^2}{(x-y)}$$

$$\Rightarrow K_{sp}K_h = xy^2$$

If:

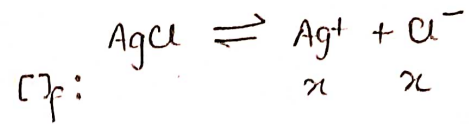
- Basic Medium introduced ⇒ Solubility of AgCN ↓
- Acidic Medium introduced ⇒ solubility of AgCN ↑

f base radical weak (like NH₄⁺) instead of acid radical (like CN⁻)

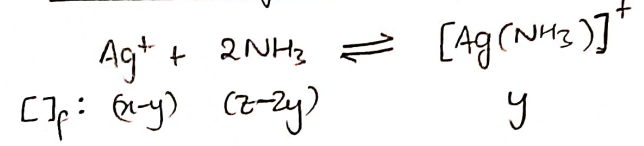
- Basic Medium introduced ⇒ Solubility ↑
- Acidic Medium introduced ⇒ Solubility ↓

Solubility of AgCl in aq. NH₃

Let initial conc. of NH₃ = z



* Ag⁺ reacts with NH₃ to form Tollen's Reagent (very stable)



Since product very stable

$$(z-2y) \sim (z-2x)$$

At eq, [Ag⁺] = (x-y)
 [NH₃] = (z-2x)
 [Ag(NH₃)₂⁺] = y
 [Cl⁻] = x

$$K_{sp} = x(x-y) \quad K_f = \frac{x}{(x-y)(z-2x)^2}$$

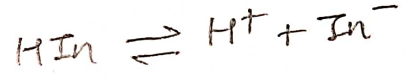
$$K_{sp}K_f = \frac{x^2}{(z-2x)^2}$$

Acid-Base Tit

Read graphs from notes

1) Acidic Indicator (HIn)

eg:- Phenolphthalein (HPh)



$$K_{In} = \frac{[H^+][In^-]}{[HIn]} \Rightarrow pH = pK_{In} + \log \left(\frac{[In^-]}{[HIn]} \right)$$

2) Basic Indicator (InOH)

eg:- Methyl orange (MOH)

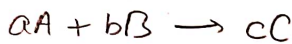
$$pOH = pK_{In} + \log \left(\frac{[In^-]}{[InOH]} \right)$$

Working Range

Acidic In: $pK_{In}-1 \leq pH \leq pK_{In}+1$

Basic In: $pK_{In}-1 \leq pOH \leq pK_{In}+1$

CHEMICAL KINETICS



$$ROR = \left(\frac{1}{a}\right)\left(\frac{-dA}{dt}\right) = \left(\frac{1}{b}\right)\left(\frac{-dB}{dt}\right) = \left(\frac{1}{c}\right)\left(\frac{dC}{dt}\right)$$

Rate of disappearance of A = $\frac{dA}{dt}$

Rate of appearance of C = $\frac{dC}{dt}$

Factors affecting ROR

1) Nature of Reactant

2) Temp. $ROR \propto T^n$

3) Surface Area $ROR \propto S.A$

2) Conc. of Reactant

4) Catalyst

5) Presence of light (if req.)

$ROR \propto (\text{Intensity of light})$

Orders can be fractional but Molecularity can NOT fractional

(ii) Order of complex rxn is determined by the slowest step - (rate determining step)
 { i.e. treating the step as the elem. rxn used to write Rate law Exp. }

First order Kinetics

1) $kt = \ln(A_0) - \ln(A)$ $\left\{ \frac{-dA}{dt} = k[A] \right\}$

2) $t_{1/2} = \frac{\ln(2)}{k}$

$t_{10\%} = t_{1/2} \times \left(\frac{10}{3}\right)$

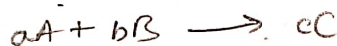
$t_{99\%} = t_{1/2} \times \left(\frac{10}{3}\right)^2$

$t_{99.9\%} = t_{1/2} \times \left(\frac{10}{3}\right)^3$

NOTE:

3) $t_{av} = \frac{1}{k}$

Rate Law & order



$ROR = k[A]^p[B]^q$

k → Rate const. of

p → order of rxn wrt A

q → order of rxn wrt B

Order of rxn = (p+q)

(iii) Elementary rxns (single step)

$p=q$ & $q=b$

(Law of Mass Action)

(ii) Molecularity - # molecular species participating in elementary rxn.
 It is not defined for complex rxns.
 For elem. rxns, Order = Molecularity

Second order Kinetics

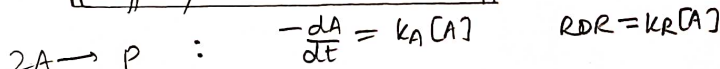
(if conc. of reactants is diff-)



i: a b

$kt = \left(\frac{1}{a-b}\right) \ln\left(\frac{a-x}{b-x}\right) \left(\frac{b}{a}\right)$

Coeff of ROR & RDA(A)



$ROR = \frac{1}{2} \left(\frac{-dA}{dt}\right) \rightarrow \boxed{k_R = 2k_A}$

Unless specified, report k_A !

Calc. of 1st order
Rean using diff. parameters

$$kt = \ln \left(\frac{X_{\infty} - X_0}{X_{\infty} - X_t} \right)$$

X_{∞} - Val. of parameter @ $t = \infty$
 X_t - Val. of parameter @ $t = t$
 X_0 - Val. of parameter @ $t = 0$

① Decomp. of H_2O_2 in terms of $KMnO_4$ used

X = Vol. of $KMnO_4$ used.

Since no H_2O_2 left at $t = \infty$,

$$\Rightarrow X_{\infty} = 0 \Rightarrow kt = \ln \left(\frac{X_0}{X_t} \right)$$

② Decomp. of H_2O_2 in terms of O_2 produced

X = Vol. of O_2 produced

Since no O_2 at $t = 0 \Rightarrow X_0 = 0$.

$$\Rightarrow kt = \ln \left(\frac{V_{\infty}}{V_{\infty} - V_t} \right)$$

③ Hydrolysis of Ethyl Acetate in terms of $NaOH$ used

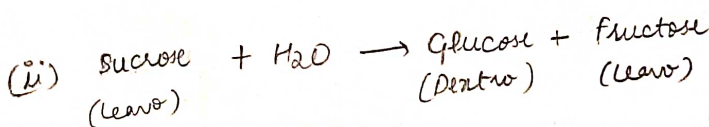
X = Vol. of $NaOH$ used.

④ Hydrolysis of Sucrose

X = Observed rotation (θ)

NOTE: (i) $\theta = \alpha LC$

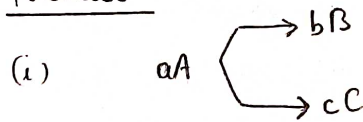
- α - specific rotation
- L - length of tube (in decimeter)
- C - conc. of sample (in g/ml)



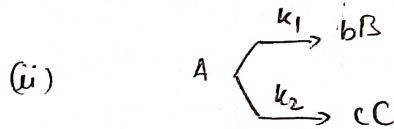
Parallel & Series Rean
(1st order kinetics)

2

① Parallel



$$A_0 = A_t + \left(\frac{a}{b}\right) B_t + \left(\frac{a}{c}\right) C_t$$



$$k_{net} = k_1 + k_2 \Rightarrow \frac{1}{(t_{1/2})_{net}} = \frac{1}{(t_{1/2})_1} + \frac{1}{(t_{1/2})_2}$$

$$A = A_0 e^{-(k_1+k_2)t}$$

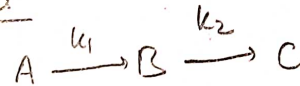
$$B = \frac{bk_1}{(k_1+k_2)} A_0 [1 - e^{-(k_1+k_2)t}]$$

$$C = \frac{ck_2}{(k_1+k_2)} A_0 [1 - e^{-(k_1+k_2)t}]$$

NOTE:

$$\frac{B}{C} = \left(\frac{b}{c}\right) \left(\frac{k_1}{k_2}\right)$$

② Series



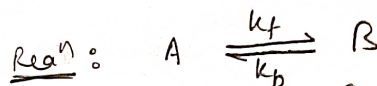
$$t_{max} = \frac{1}{(k_2 - k_1)} \ln \left(\frac{k_1}{k_2} \right)$$

$$B_{max} = A_0 \left(\frac{k_1}{k_2} \right) \left(\frac{k_2}{k_2 - k_1} \right)$$

Equilibrium
(1st order kinetics)

$$ROR = R_f - R_b$$

$$k = k_f + k_b$$



$t=0$: a 0

$t=t$: $(a-x)$ x

$t=t_{eq}$: $(a-x_e)$ x_e

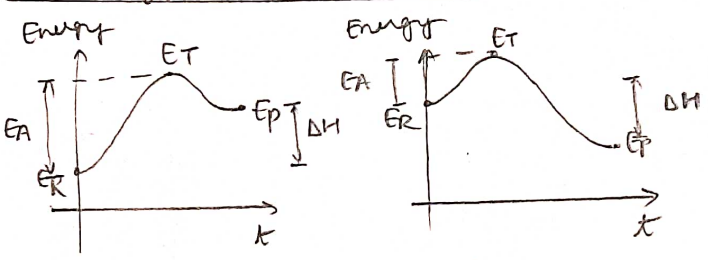
$$(k_f + k_b) t = \ln \left(\frac{x_e}{x_e - x} \right)$$

Effect of T on ROR

$$R(T+\Delta T) = R(T) \alpha^{\frac{\Delta T}{10}}$$

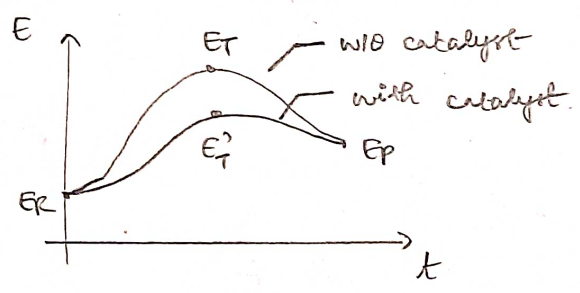
temp. coeff $\in [A, B]$

Activation Energy & Effect of Catalyst



- E_R - Energy of Reactant
- E_P - Energy of Product
- E_T - Threshold Energy
- E_A - Activation Energy

NOTE: E_A (fwd rxn) = E_A
 E_A (bwd rxn) = $E_A - \Delta H$



NOTE: ① Catalyst doesn't change energy of reactant & product

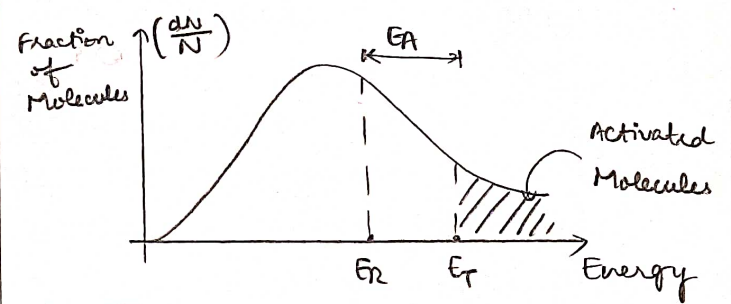
② Catalyst does not change ΔH & ΔG (Thus, also the spontaneity of rxn)

③ Catalyst does not change K_{eq} . It brings eq. faster.

Effective

Activated Molecules.

Molecules whose energy $\geq E_T$



(Fraction of Effective molecules) = $e^{-E_A/RT}$

Arrhenius Eqn

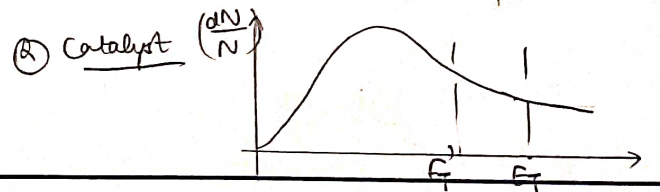
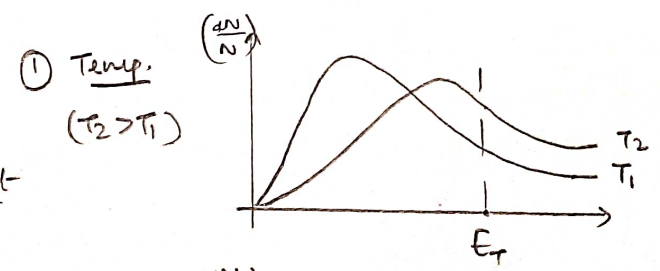
$$k = A e^{-E_A/RT}$$

Rate const. $\left\{ \begin{array}{l} \text{Arrhenius const./} \\ \text{Collision factor/} \\ \text{Pre-exponential factor} \end{array} \right.$

$$\Rightarrow \log(k) = \log(A) - \frac{E_A}{2.303RT}$$

$$\Rightarrow \log\left(\frac{k_2}{k_1}\right) = \frac{E_A}{2.303R} \left[\frac{1}{T_1} - \frac{1}{T_2} \right]$$

k_i - Rate const at temp: T_i



Radioactivity (Study from package)

Activity $A = -\frac{dN}{dt} = \lambda N$ — # nuclei at time 't'
 decay const. (independent of temp.)

NOTE: No significance of Arrhenius eqⁿ in radioactivity.

Units: 1 Ci = 3.7 x 10¹⁰ dps (disintegrations per sec.)
curie ✓

1 Bq = 1 dps (SI)

Becquerel ✓

• specific Activity - Activity of 1g radioactive sample.

$\lambda t = \ln\left(\frac{N_0}{N_t}\right)$

$N_0 = \left(\frac{W_0}{M}\right) (N_A) = n_0 N_A$
 $\Rightarrow \frac{A_0}{A} = \frac{N_0}{N} = \frac{n_0}{n} = \frac{w_0}{w}$

- Half-life - $t_{1/2} = \frac{0.693}{\lambda}$

- Avg. life - $t_{av} = \frac{1}{\lambda} = 1.44 t_{1/2}$

Internal Energy

$$\Delta U = nC_v \Delta T \quad (C_v - \text{molar specific heat capacity})$$

NOTE: (i) This formula is only valid when $n = \text{const.}$

(ii) For solids & liq,

$$\Delta U = ms \Delta T \quad (s \rightarrow \text{specific heat capacity})$$

Work

{ By sys = -ve
On sys = +ve }

$$dW = -P_{ext} dV$$

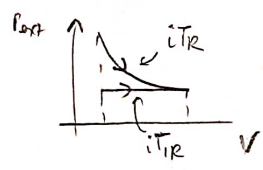
iT_R: $W = -nRT \ln\left(\frac{V_2}{V_1}\right) = -nRT \ln\left(\frac{P_1}{P_2}\right)$

iP_R: $W = -P_{ext} \Delta V$

iV_R: $W = 0 \quad (\Delta V = 0)$

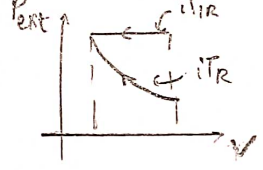
IR: $W = -P_{ext} \Delta V$

NOTE: (i) During expansion



$$W_{iT(R)} > W_{iP(R)}$$

During contraction



$$W_{iT(R)} < W_{iP(R)}$$

(ii) $W = 0$ when gas expands in vacuum (free expansion)

First Law

$$\Delta U = q + w$$

{ Heat given to sys: $q = +ve$
Heat released from sys: $q = -ve$ }

Enthalpy (H)

$$H = U + P_{ext} V$$

$$\Delta H = \Delta U + \Delta(P_{ext} V)$$

for a reversibly occurring reaction (NOT necessarily a reversible reaction)

$$\Delta H = \Delta U + \Delta n_g RT$$

$$\left\{ \begin{aligned} \Delta H = nC_p \Delta T &\Rightarrow \Delta H = q_p \\ \Delta U = nC_v \Delta T &\Rightarrow \Delta U = q_v \end{aligned} \right\}$$

Relⁿ b/w C_p & C_v

$$C_p - C_v = R$$

$$\gamma = C_p / C_v$$

Degrees of Freedom (f)

$$\gamma = 1 + \left(\frac{2}{f}\right)$$

$$C_p = \frac{\gamma R}{(\gamma - 1)}$$

$$C_v = \frac{R}{(\gamma - 1)}$$

Atomicity	Mono	Di	Tri (linear)	Tri (Non-linear)
f :	3	5	5	6
(+2)	5	7	7	8
Vibrational				

NOTE: for a mix. of gases G_1, G_2, \dots, G_m .

$$C_p^{\text{mix}} = \frac{\sum n_i C_{p_i}}{\sum n_i}$$

$$C_v^{\text{mix}} = \frac{\sum n_i C_{v_i}}{\sum n_i}$$

$$\gamma^{\text{mix}} = (C_p^{\text{mix}} / C_v^{\text{mix}}) = \left(\frac{\sum n_i C_{p_i}}{\sum n_i C_{v_i}} \right)$$

Polytropic Process

$$PV^\alpha = \text{const.}$$

if $\alpha = \gamma$, process is known as Adiabatic Process

$$W = \frac{P_2 V_2 - P_1 V_1}{(\alpha - 1)}$$

NOTE: (i) for reversible AdB.

$$\begin{aligned} PV^\gamma &= \text{const.} \\ TV^{(\gamma-1)} &= \text{const.} \\ PT^{(\frac{\gamma}{\gamma-1})} &= \text{const.} \end{aligned}$$

but $q=0$ for any AdB process whether occurring reversibly or irreversibly.

$$(ii) \quad C = C_v + \frac{R}{1-\alpha}$$

molar specific heat capacity.

Second Law

$$\Delta S_{\text{sys}} + \Delta S_{\text{surr}} > 0$$

for irreversible process.

$$\Delta S_{\text{sys}} + \Delta S_{\text{surr}} = 0 \text{ for reversible process}$$

NOTE: $(\Delta S_{\text{universe}} / \text{isolated system}) \Leftrightarrow (\text{Process is spontaneous})$

Entropy -
$$\Delta S = \int \frac{dq_{\text{rev}}}{T}$$

NOTE: (i) S: Gas > Liq. > Solid

- (ii) S \propto (Mass & size)
- (iii) S \propto Mol. wt.
- (iv) S \propto Atomicity

Entropy during Phase Change

$$\Delta S = \frac{\Delta H_{\text{sys}}(\text{process})}{T_{\text{process pt.}}}$$

Process - melting, boiling, sublimation

Entropy during TdD Process

$$\begin{aligned} \Delta S_{\text{sys}} &= nC_v \ln\left(\frac{T_2}{T_1}\right) + nR \ln\left(\frac{V_2}{V_1}\right) \\ &= nC_p \ln\left(\frac{T_2}{T_1}\right) + nR \ln\left(\frac{P_1}{P_2}\right) \end{aligned}$$

$$\Delta S_{\text{surr}} = \frac{q_{\text{surr}}}{T_{\text{surr}}} = -\frac{q_{\text{sys}}}{T_{\text{surr}}}$$

for Rev. process, $\Delta S_{\text{surr}} = -(\Delta S_{\text{sys}})$

IR: IT: $\Delta S_{\text{surr}} = \frac{W}{T_{\text{surr}}} = \frac{-P_{\text{ext}}(V_2 - V_1)}{T_{\text{surr}}}$

iP: $\Delta S_{\text{surr}} = -\frac{\Delta H_{\text{sys}}}{T_{\text{surr}}} = \frac{-nC_p(T_2 - T_1)}{T_2}$

iV: $\Delta S_{\text{surr}} = -\frac{\Delta U_{\text{sys}}}{T_{\text{surr}}} = \frac{-nC_v(T_2 - T_1)}{T_2}$

NOTE:

	ΔS_{sys}	ΔS_{surr}
AdB _R	0	0
AdB _{IR}	$\left(nC_v \ln\left(\frac{T_2}{T_1}\right) + nR \ln\left(\frac{V_2}{V_1}\right) \right)$	0

Gibbs Free Energy

$$dG = V dP - S dT$$

for T=const.

$$\Delta G = nRT \ln\left(\frac{P_2}{P_1}\right)$$

$$\Delta G = \Delta G^\circ + RT \ln(Q)$$

@ eq. $\Delta G = 0$

↓

$$\Delta G^\circ = -RT \ln(K)$$

NOTE (i) $(\Delta G)_{P,T} = \Delta H - T \Delta S$

(ii) $(\Delta G)_{P,T} < 0 \Leftrightarrow \text{Rev}^\circ \text{ is spontaneous}$



Thermochemistry

$$1) \Delta H_r = \sum \Delta H_f(\text{Products}) - \sum \Delta H_f(\text{Reactants})$$

$$= \sum \text{BE}(\text{Reactants}) - \sum \text{BE}(\text{Products})$$

$$2) (\Delta H_r)_{T_2} - (\Delta H_r)_{T_1} = \Delta C_p (T_2 - T_1)$$

$$3) \Delta S_{T_2} - \Delta S_{T_1} = \Delta C_p \ln\left(\frac{T_2}{T_1}\right)$$

$$ds = \frac{dq_{rev}}{T} = \frac{\Delta C_p dT}{T}$$

$$4) \Delta H_{neu}^{\circ} = \Delta H_{ionisation}^{\circ} + \Delta H_{rean}^{\circ}$$

-57.1 kJ/mol
OR -13.7 kcal/mol



$$5) \text{Resonance Energy} = \Delta H_f(\text{observed}) - \Delta H_f(\text{Theoretical})$$

(Comp. with Resonance) (Comp. w/o Resonance)

